

**Optimization of waste heat utilization in
oil field development employing a
supercritical Organic Rankine Cycle (ORC)
for electricity generation - with Chevron Technology
Venture Emerging Energy**

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Outline

- I. Waste heat utilization
- II. ORC power generation
- III. Optimization methodology
- IV. Cycle sensitivity analysis
- V. Conclusion

Questions to address:

What is waste heat?

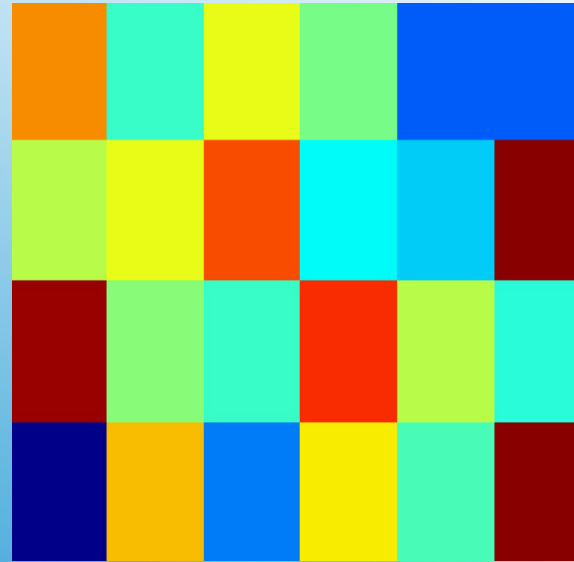
How do I utilize it?

How much power?

Shall we go for it?

Waste heat utilization

Revolution



Evolution

Heat

Conserved quantity which only knows one direction!

Thermodynamic cycles transfer heat into a more valuable energy forms. Around 85 % of the worlds electricity demand is generated this way! How can heat be considered waste? Because the value of the energy is depending on the existing thermal contrast from which the energy quality is derived! Wrong?

1st Law = "Value of energy" 2nd Law = "Temperature & Irreversibility"
 $dU = \delta Q + \delta W$ $dS = \delta Q/T + \delta W/T \geq 0$

Heat source Temperature [°C]	450	300	150
Heat sink Temperature [°C]	20	20	20
Carnot efficiency [%]	59	49	31

Waste heat accounts for 60 % of the industrial thermal pollution in the U.S.

High : > 650 °C
Medium: ~ 330 °C
Low: < 230 °C

ORC power generation

Utilizing heat by employing the Clausius-Rankine thermodynamic cycle with carbon based fluids.

Electric power generation from:

- Geothermal
- Biomass
- Industrial waste heat
- Solar thermal
- CHP
- Water desalination (thermal)

Why ORC?:

- Highly reliable electric power supply
- Starting from 1 kW – 100 MW
- Zero emissions
- Applicable with CHP
- Continuous power production
- Maintenance free
- Easy and fast to assemble

Minimum thermal requirements:

- $\Delta T = 60 \text{ }^\circ\text{C}$
- "Heat source nature"

**NO FUEL CONSUMPTION AND NO POLLUTION =
RENEWABLE ENERGY**

Unconventional heat source

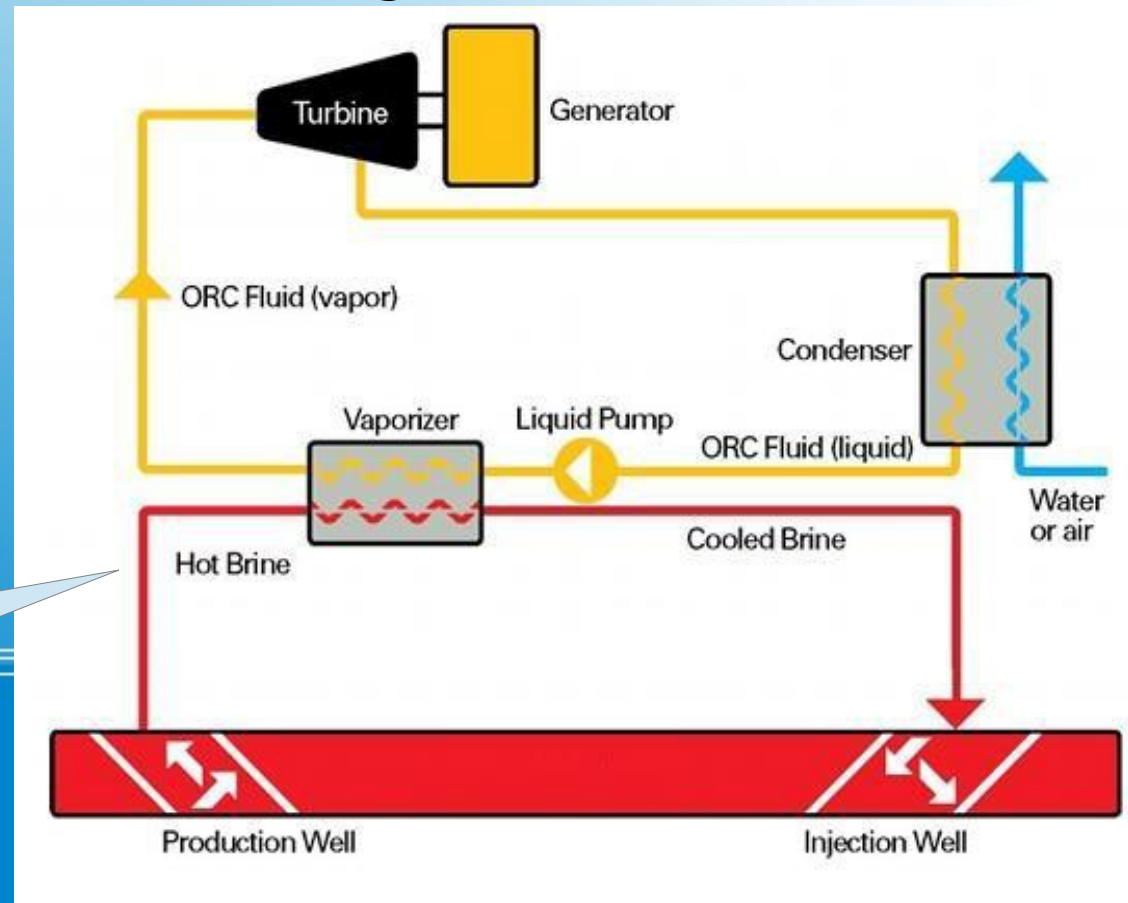
Energy companies with mature heavy and extra heavy crude oil fields employ sweeping as recovery enhancement in secondary and tertiary oil development!

High pressurized water is injected into the ground so that the brine coming out of the production well has a higher oil content.

Heat source nature:

- 150 °C
- 500 kPa
- 4.53 kg/s
- Phase fraction of 0.98
- On Chevrans' oil fields in Indonesia, Kazakhstan, Middle East and the US

Approx. 7 MW thermal power per oil well



Methodology

Design a dynamic and flexible unit configuration.

ORC plant:

- Cycle layout (Supercritical)
- Fluid and fluid properties (R134a)
- Equipment (Heat exchanger, expander, cooler, pump)

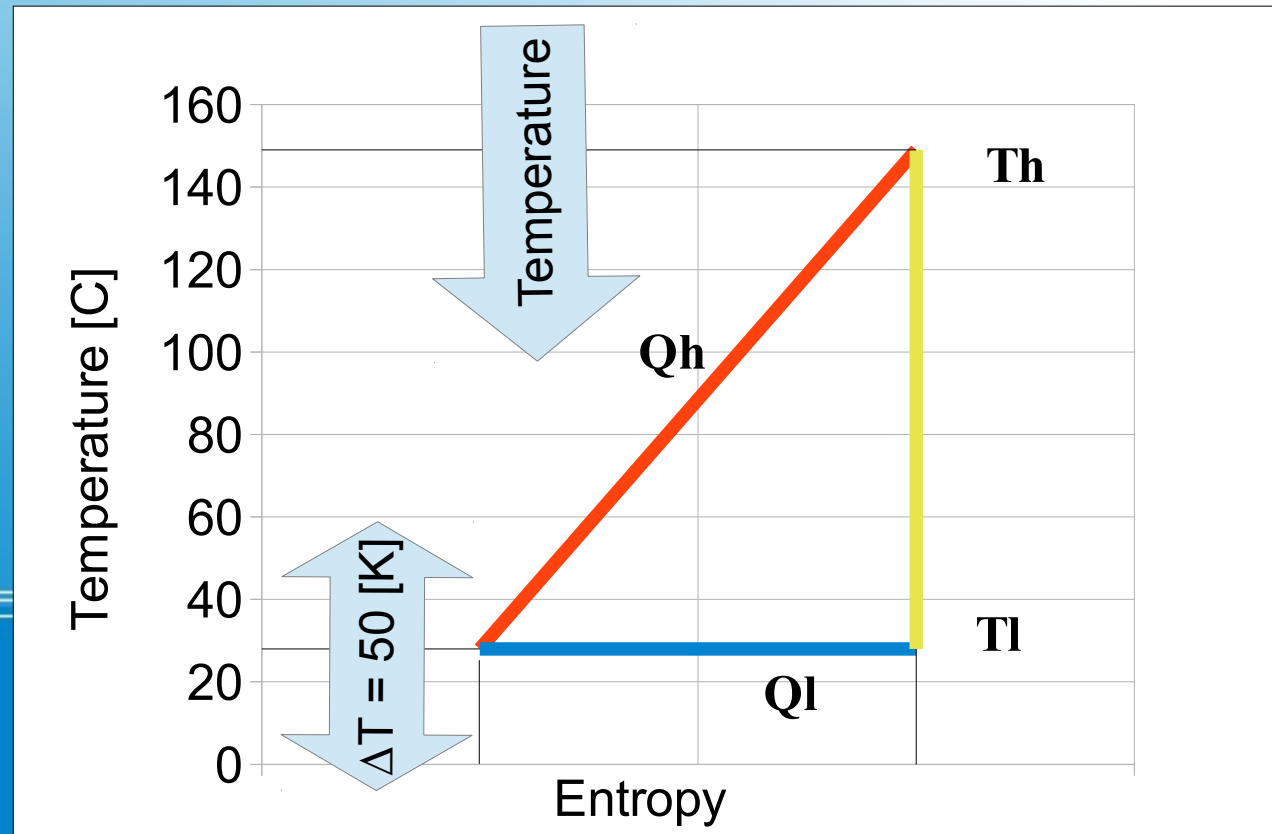
Changing boundaries:

- Thermal (Source and sink)
- Financial (Industrial size)

Organic fluid:

$$T_c = 101 \text{ }^\circ\text{C}$$

$$P_c = 4.06 \text{ MPa}$$



Cycle optimization

Adjusting the elementary variables temperature and pressure.

$$P_{\text{net}} \rightarrow \text{Max.} := Q_h - Q_l - P_{\text{Pump}} - P_{\text{Cooler}} + P_{\text{expander}}$$

Maintained by the pump speed

With:

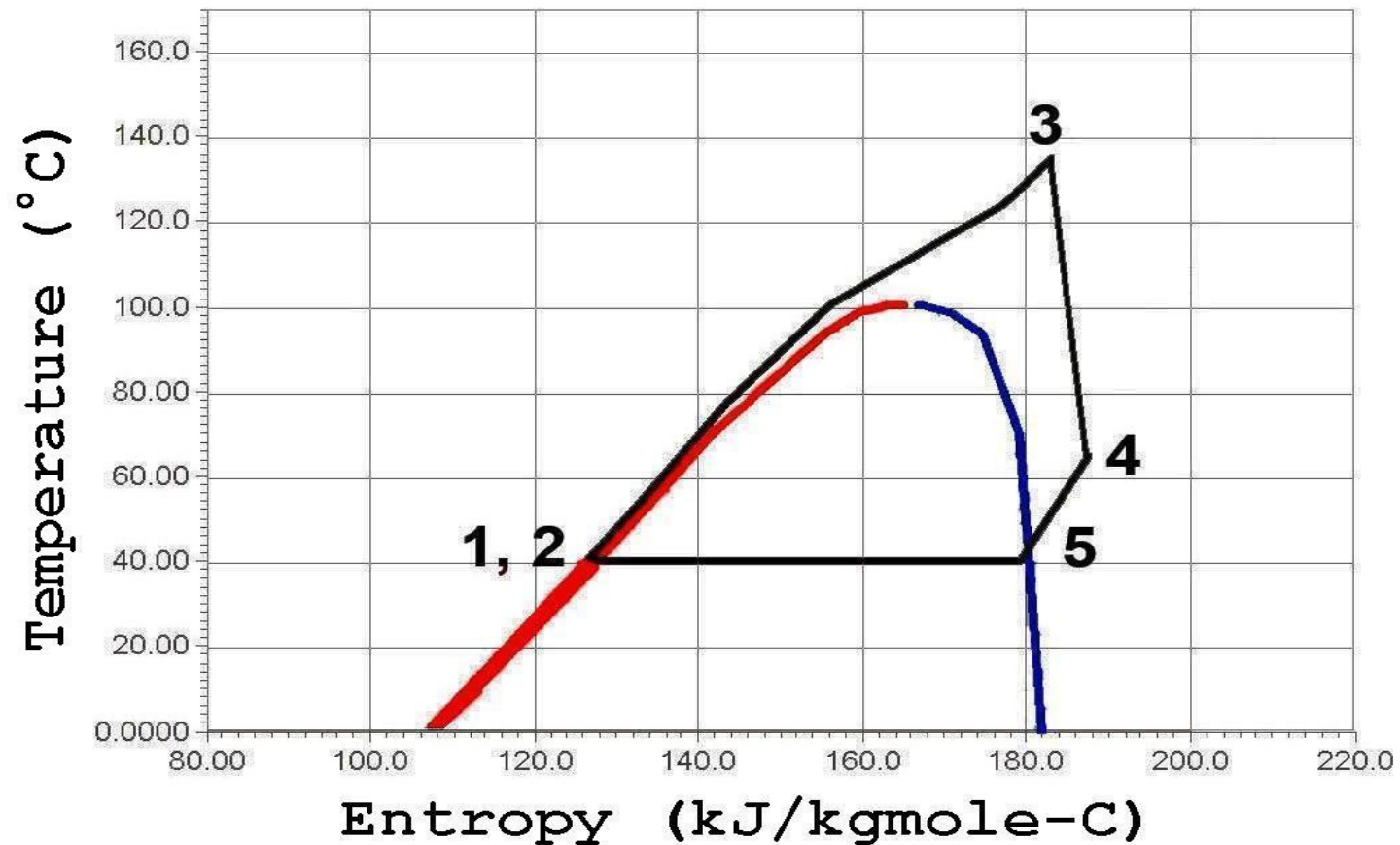
$$Q_h = m_{\text{ORC}} (h_3 - h_2) \\ = 7 \text{ MW}$$

And:

$$UA = Q_h / \text{LMTD}$$

Where:

UA = Heat transfer
Conductance



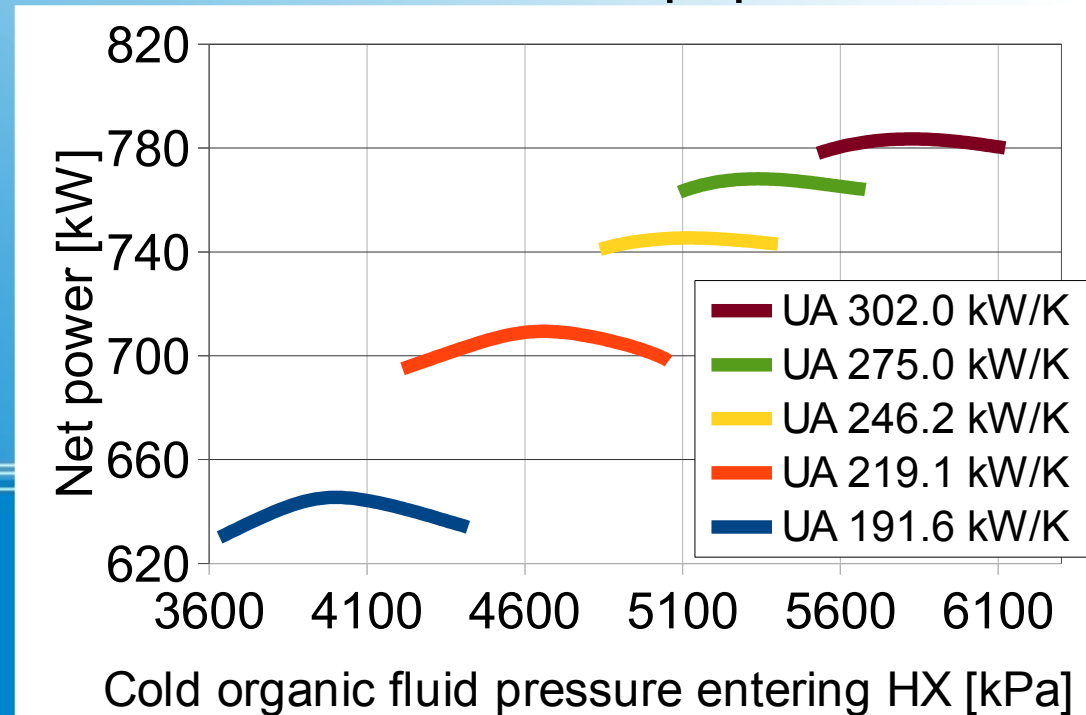
Heat Transfer

As the system is directly linked with the heat transfer: maximise the heat transfer.

- Positive “heat transfer conductance”/“organic fluid pressure” correlation
- Losses under suboptimal pressure operation higher for small heat transfer equipment than for large one
- Risk of subcritical operation for small heat transfer equipment higher than for large one

According to Karellas et al. the heat transfer improvements are governed by nonlinear supercritical fluid properties

(R134a, R227ea and R245fa - for $A = 2.5 \text{ m}^2$, here $\sim 60 \text{ m}^2$)



Power

Net power performance of the plant for changing ambients.

T_l 28 °C	Heat transfer conductance UA [kW/K]				
T_h 149 °C	191.6	219.4	246.2	275.0	302.0
Pump head [m]	ORC net power P_{net} [kW]				
293	521	551	556	558	560
Critical	-	-	-	-	-
323	531	578	591	565	569
343	531	589	611	620	624
373	574	614	629	633	636
393	524	599	634	651	659
413	505	595	638	659	669

T_l 19 °C	Heat transfer conductance UA [kW/K]				
T_h 149 °C	191.6	219.4	246.2	275.0	302.0
Pump head [m]	ORC net power P_{net} [kW]				
293	630	648	649	652	654
Critical	-	-	-	-	-
323	644	678	690	622	685
343	645	695	709	741	717
373	637	708	734	745	750
393	633	708	741	755	762
413	630	705	745	763	772

494	589	639	663	675
480	581	636	664	679
465	571	631	663	680
447	560	623	660	681
432	552	615	654	667
5	8.8	9.1	9.5	9.7

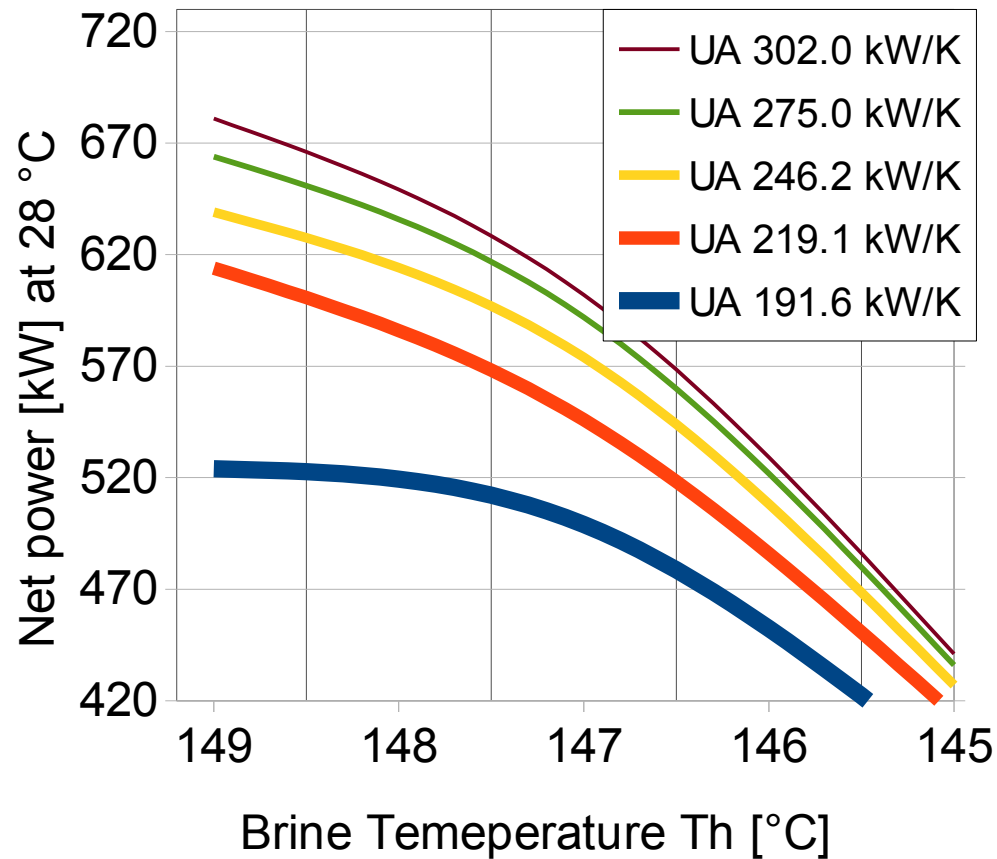
T_l 10 °C	Heat transfer conductance UA [kW/K]				
T_h 149 °C	191.6	219.4	246.2	275.0	302.0
Pump head [m]	ORC net power P_{net} [kW]				
293	751	758	760	762	763
Critical	-	-	-	-	-
323	777	787	792	794	795
343	790	803	808	812	812
373	807	824	832	835	837
393	808	832	842	847	849
413	808	838	850	856	860
433	801	839	855	862	867
453	796	837	857	867	872
473	787	834	857	867	875
493	780	827	854	868	876
513	772	819	849	865	875
Cycle η [%]	11.5	12.0	12.2	12.5	12.5

612	698	745	767	778
600	691	743	768	782
590	662	731	767	783
578	674	730	764	783
563	665	726	758	780
0	10.1	10.6	11.0	11.2

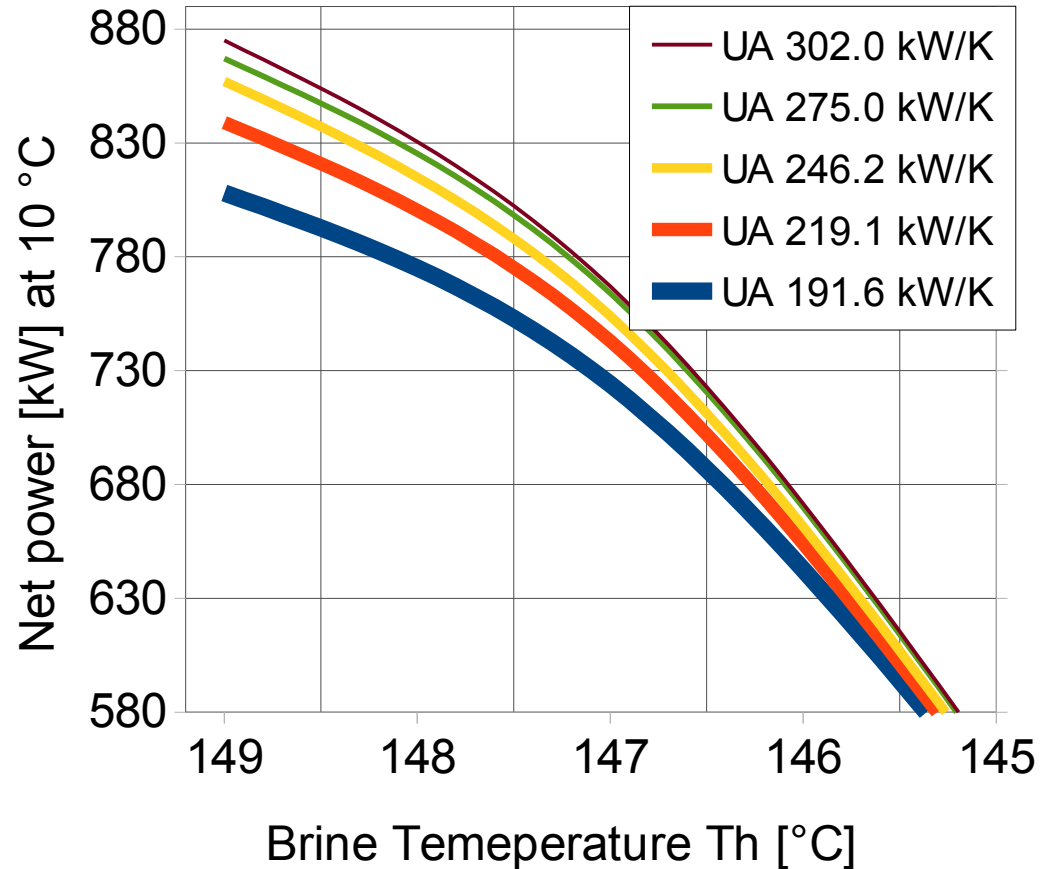
Up to -27 % in power for T_l changes
 Up to -2.2 % in η for UA changes
 Up to -10 % in power for p changes

optimization methodology- **Cycle sensitivity analysis** - Conclusion

Deteriorating brine temperature



At 28 °C ambient temperature



At 10 °C ambient temperature

HX choice determined by:

- Heat source temperature deterioration rate
- Value of additional “free” power
- Cycle flexibility

Conclusion

1. Cycle working pressure and heat exchanger surface area have to increase proportionally.
2. Low cost equipment and aggressive design vs. high performance flexible long term performance ORC.
3. Power and efficiency improvements just by adjusting the cycle working Pressure.
4. Deviations from the ideal operation under hot ambient conditions higher than under cold ones.



5. ORC power generation is always “green” because it does not require fossil fuels!

Thank you – Questions?

References:

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